



Getaran Pilar Jembatan Progo

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RINGKASAN

Kondisi pilar jembatan Progo dievaluasi dari segi perilaku dinamik dengan mengadakan pengukuran getaran di lapangan.

Analisa teoritik dimodifikasi dengan parameter dinamik sehingga diperoleh tinggi efektif pilar terhadap titik jepit dalam pondasi tiang sumuran.

Titik jepit pondasi dalam arah melintang dan memanjang jembatan menjadi kriteria untuk kondisi stabilitas pilar.

Stabilitas pilar menjadi dasar dalam menentukan cara pengamanan dan perkuatan pilar.

SUMMARY

The Conditions of Progo bridge piers are evaluated based on their dynamic behaviour, which is obtained through vibration measurement on the site.

The theoretical analysis is modified by using the dynamic parameters, revealing the effective pier height to the poin offixity of the bore pile foundation.

The fixity of the foundation in transverse and longitudinal directions is the main criteria in the determining the stability of the piers.

The pier stability is the basic principle for the protection and strengthening recommendation of the piers.

1. PENDAHULUAN

Dalam rangka penelitian kondisi pilar jembatan Progo-Bantar di Jogjakarta, telah dilakukan pengujian pengukuran getaran pada pilar dan bangunan atas jembatan Progo oleh tim Puslitbang Jalan. Data getaran telah digunakan sebagai data masukan dalam analisis kondisi aktual pondasi pilar.

2. METODA PENELITIAN GETARAN

Penggerusan sungai di lokasi pilar-pilar telah menyebabkan terbukanya sambungan pengecoran beton yang semula berada pada ketinggian dasar sungai. Kedalaman gerusan dasar sungai sebesar kurang lebih 6 m (arah Wates) dan 3 m (arah Jogja) telah mengurangi kedalaman terbenamnya pondasi tiang. Getaran pilar dan bangunan atas akibat gaya arus dengan atau tanpa kombinasi beban lalu lintas pada jembatan, telah diukur pada puncak pilar dan

tengah bentang dalam tiga arah sumbu ortogonal X, Y dan Z. Pengamatan getaran mengungkapkan besarnya gerakan pilar serta kekakuan pilar yang masing-masing dinyatakan dalam simpangan dinamik (mm) dan frekuensi (Hertz). Berdasarkan frekuensi terukur kemudian dapat diadakan analisis stabilitas pilar dalam arah melintang dan memanjang, yang menyatakan kondisi aktual pilar. Hasil analisis eksperimental tersebut digunakan sebagai kriteria dalam penilaian kondisi getaran pilar.

3. KERANGKA PEMIKIRAN TEORITIK

Dalam perencanaan pondasi tiang umumnya dianggap bahwa susunan tiang secara bersama memikul momen tetapi secara individual memikul beban vertikal dan beban lateral, yang dirumuskan sebagai berikut:

$$V_i = \frac{V}{n} \pm \frac{M_x \cdot Y_i}{\sum(Y_i^2)} \pm \frac{M_y \cdot X_i}{\sum(X_i^2)}$$

$$H_i = \frac{H}{n} \quad (1)$$

dengan :

V_i = gaya aksial tiang

H_i = gaya lateral tiang

V = beban vertikal pada susunan tiang

M = momen pada susunan tiang

n = jumlah tiang

x, y = jarak tiang terhadap sumbu utama Y, X

Rumus (1) hanya berlaku untuk susunan tiang yang seluruhnya terbenam dalam tanah, sedang dalam kasus jembatan Progo tiang berada sebagian diatas dasar sungai. Dengan menganggap bahwa tanah fiktif antara dasar balok pondasi dan dasar sungai mempunyai modulus elastis $E = 0$, berat isi = 0 dan sudut geser dalam $\Phi = 0$, perhitungan dengan program 'Piling' dari BMS menghasilkan gaya aksial tiang yang lebih besar dan disesuaikan dengan pengaruh tinggi bebas tiang. Interaksi struktur tiang, gaya geser tiang dan simpangan tiang yang dihitung berdasarkan beban rencana ultimate sesuai Peraturan beban jembatan - bagian 2 dari BMS. Hasil perhitungan kombinasi pembebanan yang mendekati keadaan pengujian getaran kemudian digambar dalam grafik pada Lampiran 1 - 4. Perhitungan tipikal dengan program komputer BMS diuraikan dalam Lampiran 5.

Dari perhitungan pondasi secara teoritik diperoleh data sebagai berikut :

- titik jepit pondasi yaitu titik dimana momen maksimum dan geser nol
- titik tetap pondasi yaitu titik dimana simpangan atau lenturan nol
- titik balik yaitu titik dimana momen berubah tanda

Ikhtisar hasil perhitungan teoritik dapat disusun sebagai berikut :

- titik jepit pondasi berada minimal 8 m diatas dasar tiang sumuran
- titik tetap pondasi berada minimal 3.5 m diatas dasar tiang sumuran

- titik balik berada pada ketinggian 2 - 6 m diatas dasar sungai

Perhitungan teoritik telah dibuat berdasarkan perkiraan kedalaman gerusan dan gaya aliran sungai sehingga perlu diversifikasi dengan hasil pengamatan getaran pilar.

4. HASIL DAN PEMBAHASAN GETARAN PILAR

Dalam evaluasi getaran dianggap bahwa pilar merupakan struktur kantilever yang terjepit dalam pondasi dan bergetar sebagai bandul dengan derajat kebebasan tunggal. Gaya penggetar dalam pengujian ini berasal dari bangunan atas - beban hidup - beban aliran dan turbulensi. Respon pilar terhadap gaya penggetar adalah lenturan - simpangan pilar yang diukur pada puncak pilar dengan menggunakan alat perekam getaran.

Data rekaman getaran memberikan nilai simpangan dinamik dan frekuensi pilar yang menjadi data masukan untuk analisis dinamik. Cara analisis modal yang digunakan adalah berdasarkan hukum kekekalan energi dalam perumusan sebagai berikut :

$$\frac{1}{2} \int_0^h EI (u'')^2 dx = \frac{1}{2} \omega^2 \int_0^h m u^2 dx$$

dengan :

h = tinggi efektif pilar sampai kedalaman jepit (= $d+1.2m$)

EI = kekakuan inersia pilar terhadap sumbu utama X dan Y

u = fungsi perubahan bentuk pilar dalam mode 1 : $u = (x/h)^2$

m = masa per satuan panjang pilar

w = frekuensi sirkular pilar (= $2 \pi f$)

Masa (berat/gravitasi) dan kekakuan inersia (EI) pilar disusun dalam Tabel 1 sebagai berikut :

Tabel 1. Masa dan kekakuan inersia pilar

Pilar No	Interval (m)	Masa KNd ² /m ²	EI KNm ² .10 ⁶ memanjang- melintang	
1	0 - d d-(d+1.2)	11.31 559.08	149.216 1706.5	1882.74 (8.446)* 17476.25
2	0 - d d- (d+1.2)	11.31 612.3	149.216 1706.5	1882.74 (8.446)* 17476.25
3	0 - d d- (d+1.2)	11.31 559.08	149.216 1706.5	1882.74 (8.446)* 17476.25

Dengan cara uji coba dimana d atau kedalaman jepit tiang variabel antara 10 - 25 m diperoleh nilai frekuensi sirkular yang sesuai dengan frekuensi aktual terukur. Tinggi efektif tiang ($h = d + 1.2m$ tebal balok pondasi) adalah kriteria untuk menentukan stabilitas pondasi. Bila tiang terjepit diatas elevasi dasar pondasi maka pondasi stabil - dan bila tiang terjepit pada elevasi dasar tiang maka pondasi labil. Hasil perhitungan analisis modal disusun dalam grafik Lampiran 1-4.

Dari analisis dinamik eksperimental diperoleh data sebagai berikut :

- titik jepit pondasi yaitu titik dimana pilar efektif terbenam dalam tanah
- integritas kekakuan inersia pilar dalam arah memanjang dan melintang yang tergantung pada kesatuan struktural

Ikhtisar hasil analisis dinamik dapat disusun sebagai berikut :

- titik jepit pondasi dalam arah memanjang adalah stabil karena berada :
 - 11 m diatas elevasi dasar tiang untuk pilar no.1
 - 5.2m diatas elevasi dasar tiang untuk pilar no.2
 - 7.6m diatas elevasi dasar tiang untuk pilar no.3
- titik jepit pondasi dalam arah melintang adalah labil karena berada pada elevasi dasar tiang untuk semua pilar
- integritas pondasi dalam arah memanjang didukung oleh kesatuan tiang sumuran yang memberikan kekakuan inersia penuh (149.216 KNm².10⁶ dalam Tabel 1) terhadap sumbu utama bersama

- integritas pondasi dalam arah melintang tidak didukung karena tiang sumuran memberikan kekakuan inersia parsial yang merupakan kekakuan inersia terhadap sumbu sendiri dari masing-masing tiang (8.446 KNm².10⁶ * dalam Tabel 1)

5. KESIMPULAN DAN SARAN

5.1. KESIMPULAN

- Pilar stabil dalam arah memanjang karena merupakan kesatuan yang terikat oleh susunan perletakan bangunan atas jembatan.
- Pilar labil dalam arah melintang karena hanya terikat oleh balok pondasi di puncak pilar.

5.2 SARAN

- Perlu diadakan ikatan melintang tambahan pada semua pilar dengan salah satu cara berikut :
 - membuat dua ikatan melintang dengan jarak antar sebesar 5m - 7m pada bagian tiang sumuran yang berada diatas dasar sungai; ikatan dibuat dari batang baja dan wartelmur atau dari beton bertulang
 - membuat balok pondasi yang terbenam dalam dasar sungai dan terlindung terhadap penggerusan
- Perlu diadakan perlindungan terhadap penggerusan dasar sungai dengan salah satu cara berikut :
 - pelantain dasar sungai di lokasi pilar-pilar
 - bangunan pengendali gerusan
 - bangunan peredam arus sunagi

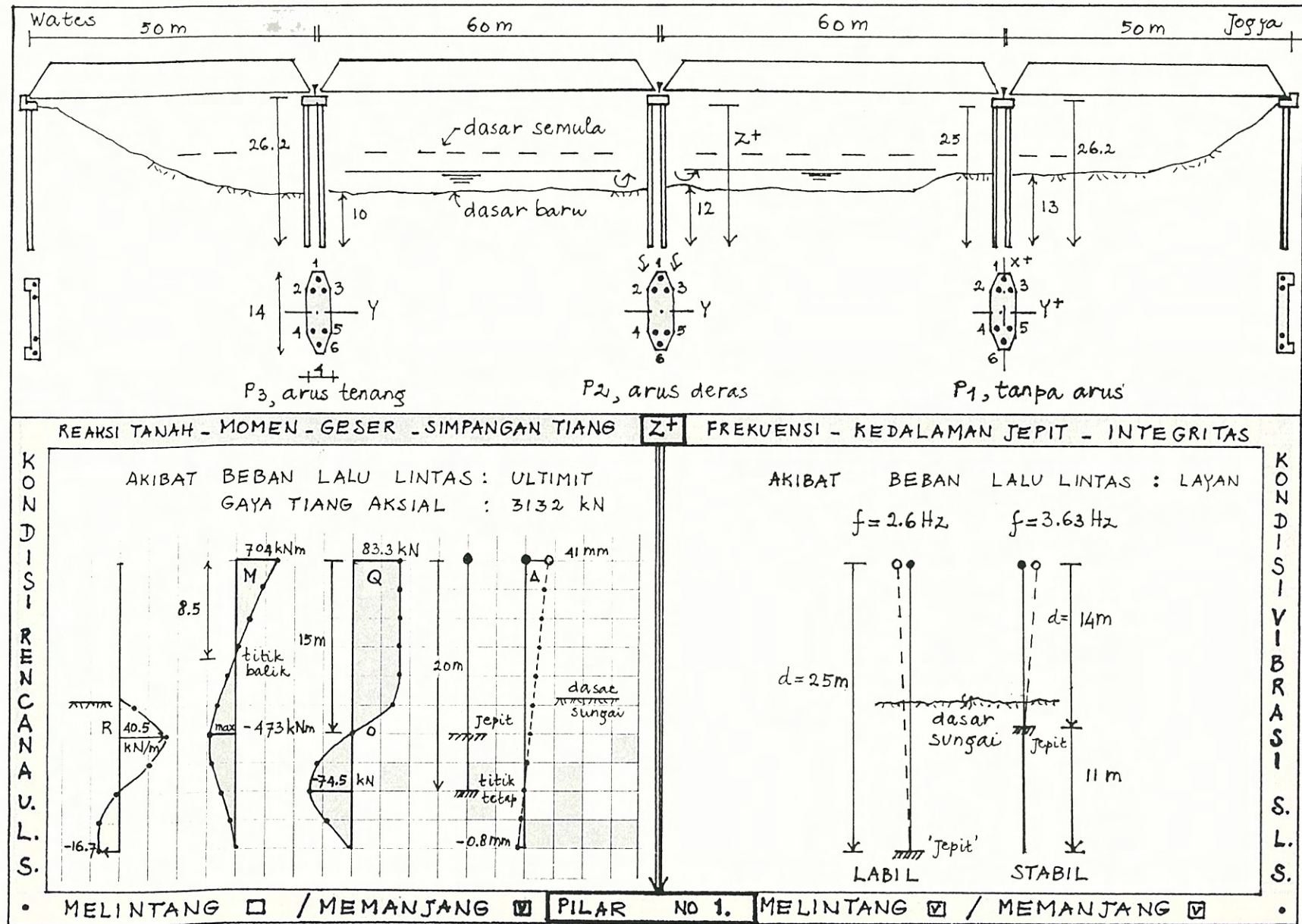
6. PUSTAKA

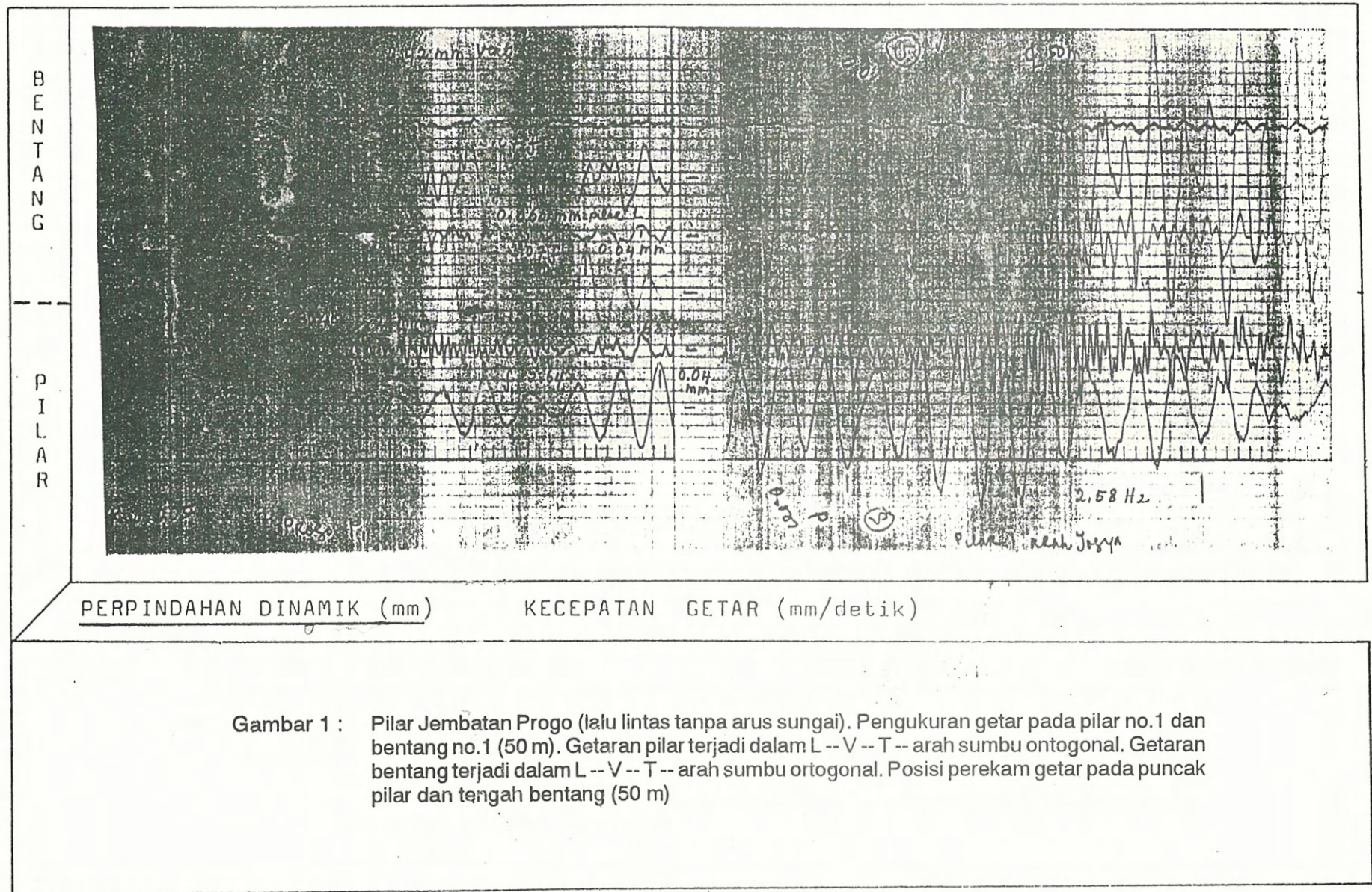
- Peraturan Beban Jembatan - Bagian 2 - BMS
- Program Piling - Lampiran Panduan BMS
- Laporan Penelitian Pengaruh Getaran Pada Pilar Jembatan - Puslitbang Jalan - 1991

Penulis :

Ir. Lanneke Tristanto, Ajun Peneliti Bidang Konstruksi Bangunan Pelengkap Jalan. Bekerja di Direktorat Bina Program Jalan, Bina Marga tahun 1970 - 1979 dan di Pusat Litbang Jalan Tahun 1979 - sekarang.

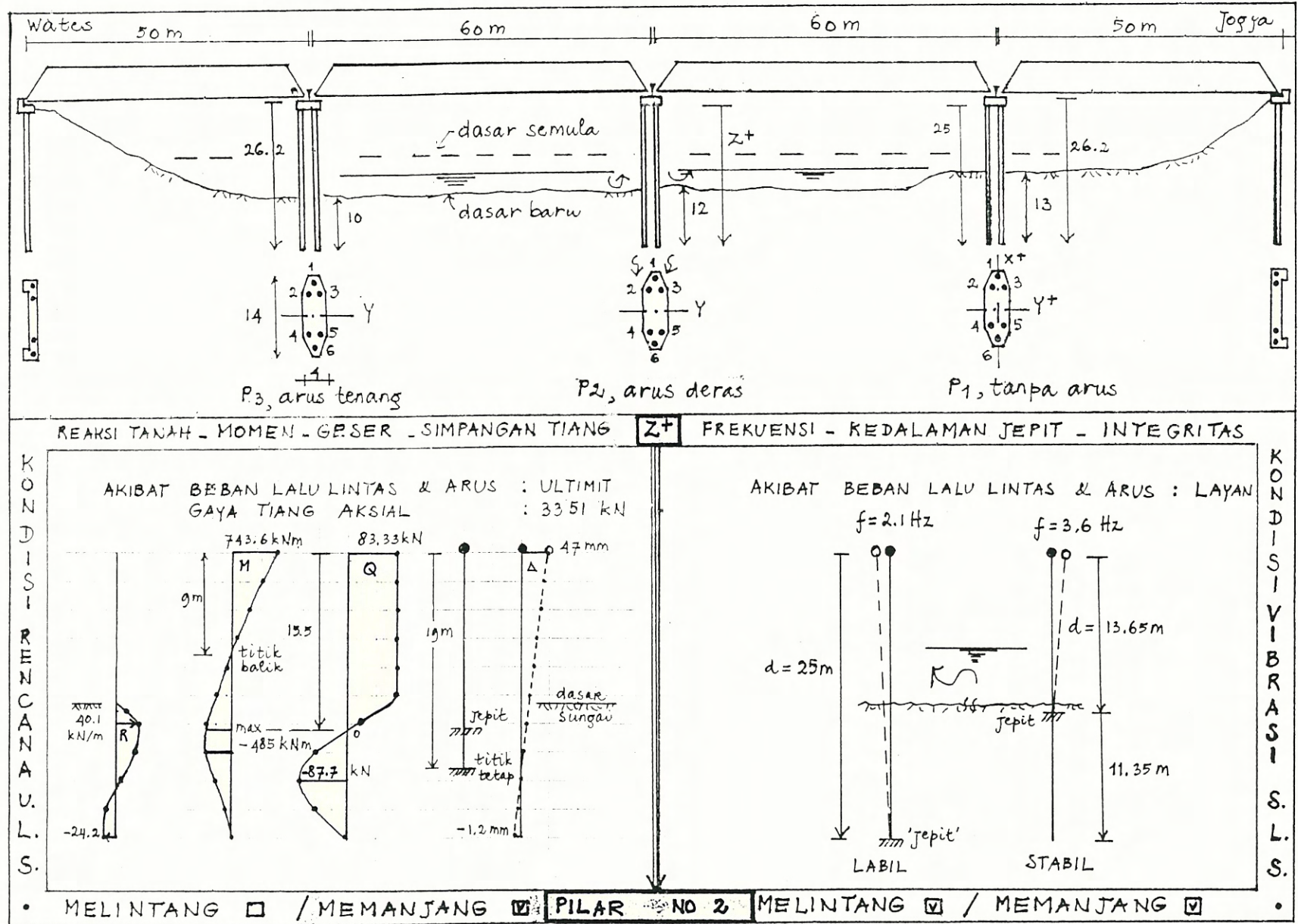
Jurnal Pusat Litbang Jalan 1 (X) Juni 1993

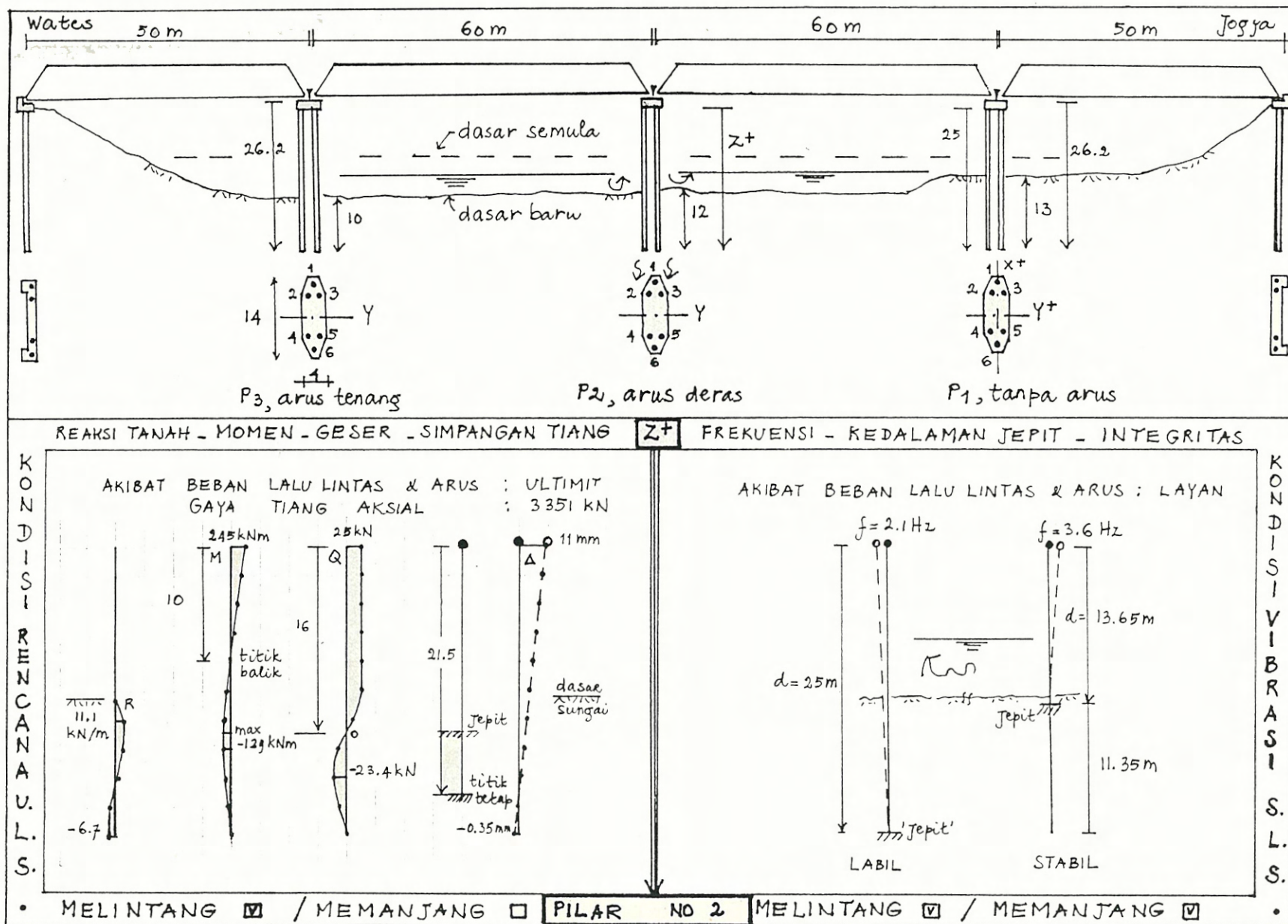




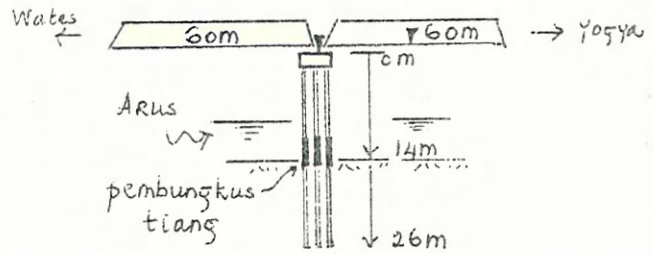
Gambar 1 : Pilar Jembatan Progo (lalu lintas tanpa arus sungai). Pengukuran getar pada pilar no.1 dan bentang no.1 (50 m). Getaran pilar terjadi dalam L -- V -- T -- arah sumbu ortogonal. Getaran bentang terjadi dalam L -- V -- T -- arah sumbu ortogonal. Posisi perekam getar pada puncak pilar dan tengah bentang (50 m)

LAMPIRAN 2 :
Pilar no.2 arah Jogja

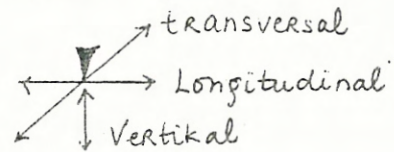




TES GETAR PILAR DAN JEMBATAN (LALU LINTAS $\equiv$ *Rangkaian  / satu  TRUK)										
No.	Jembatan	Pondasi	Tinggi Pilar(m)		Arah	Frekwensi(Hertz)		Intensitas Getar		
			bebas	tertanam		Pilar	Jembatan	Pilar	Jembatan	Dimensi
2	Progo	Tiang bor	14 m	12 m	L	3.63	—	<u>0.016</u>	0.01	Perpindah-an (mm) dinamik
					V	2.05	2.26	0.011	0.35	
					T	2.08	3.20	<u>0.017</u>	0.025	
					L					Kecepatan (mm/detik) getar
					V					
					T					

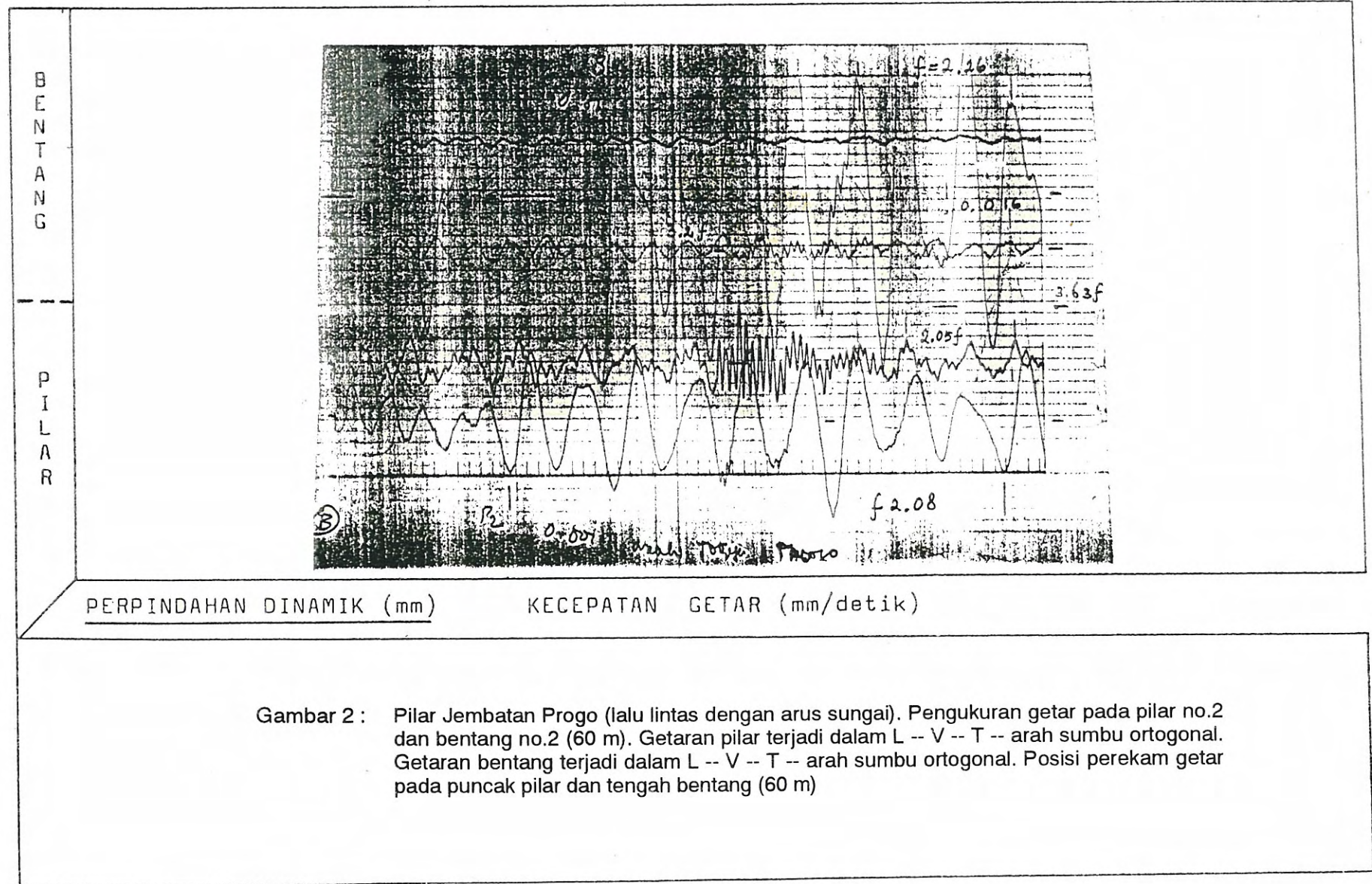


Pilar 2 arah Yogya

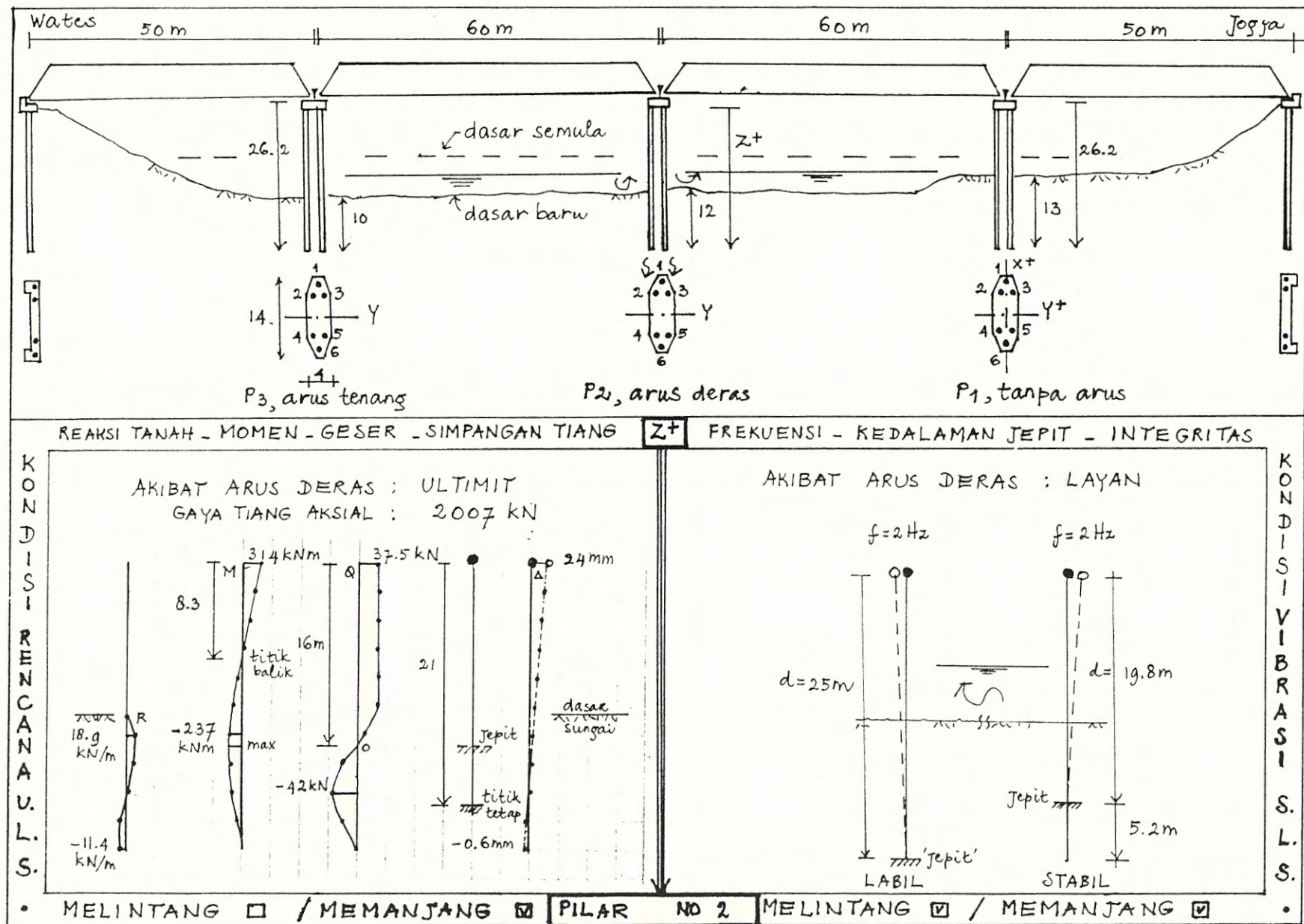


* Rangkaian lalu lintas dengan arus deras

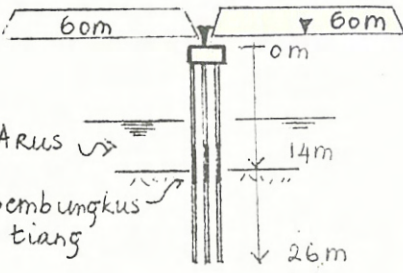




LAMPIRAN 3:
Pilar no.2 arah Jogja (khusus terhadap arus sungai)



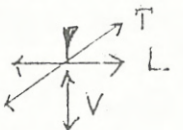
TES GETAR PILAR DAN JEMBATAN (LALU LINTAS * Rangkaian ☒ / satu ☐ TRUK)										
No.	Jembatan	Pondasi	Tinggi Pilar(m)		Arah	Frekuensi(Hertz)		Intensitas Gatar		Dimensi
			bebas	tertanam		Pilar	Jembatan	Pilar	Jembatan	
3	Progo	Tiang bor	14m	12m	L	2	—	0.008	0	Perpindah-an (mm) dinamik
					V	—	2.08	0.001	0.05**	
					T	2	—	0.002	0	
					L					Kecepatan (mm/detik) getar
					V					
					T					

Wates →  → Yogya

Arus →

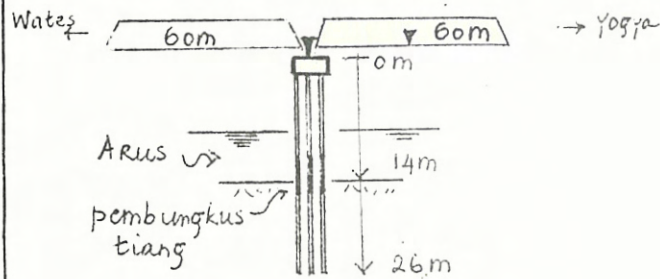
pembungkus tiang

Pilar 2 arah Yogya

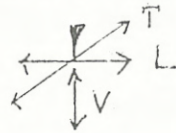


* hanya akibat arus sungai, jembatan kosong

** jembatan bergetar arah vertikal

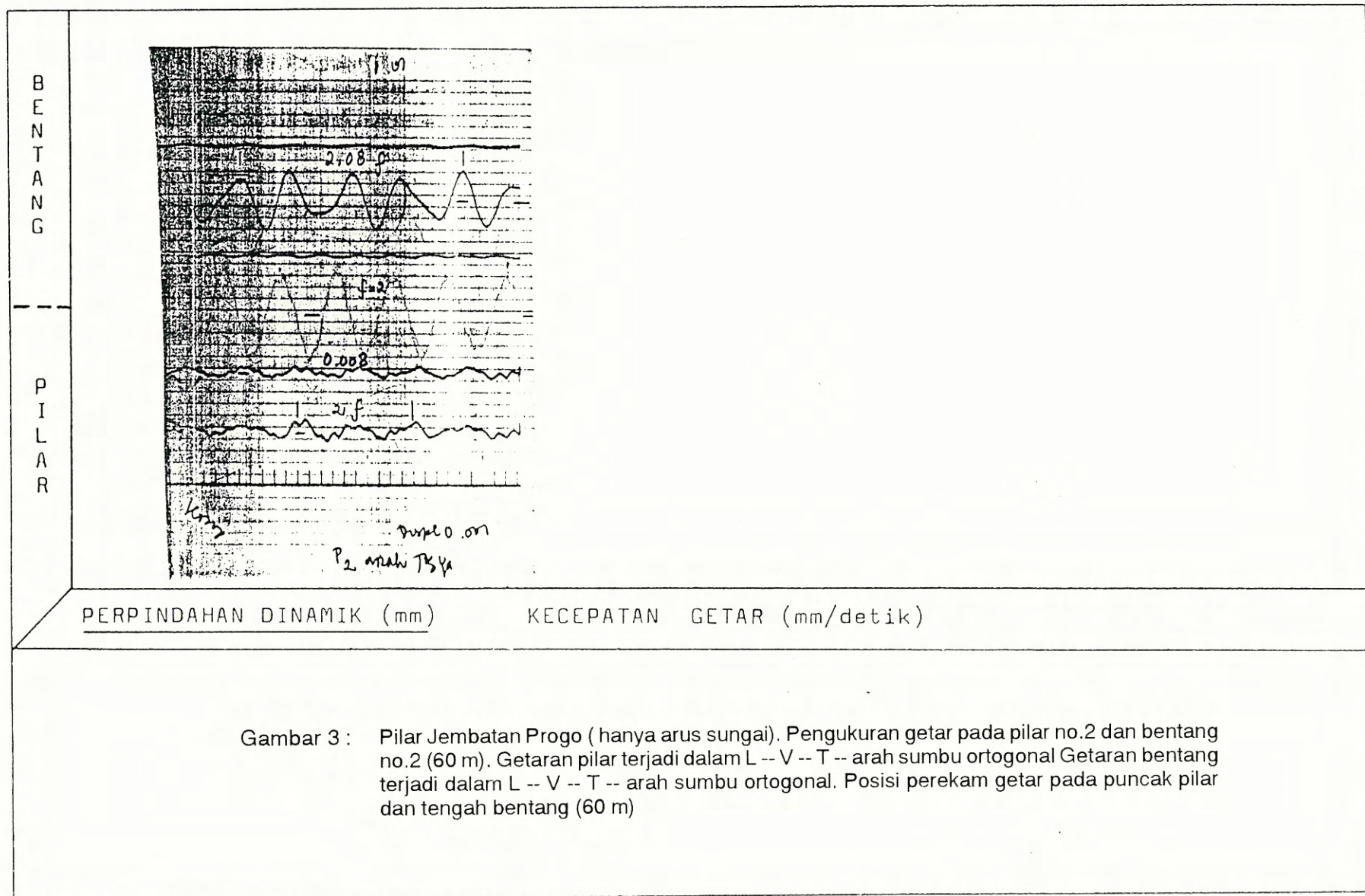


Pilar 2 arah Yogya

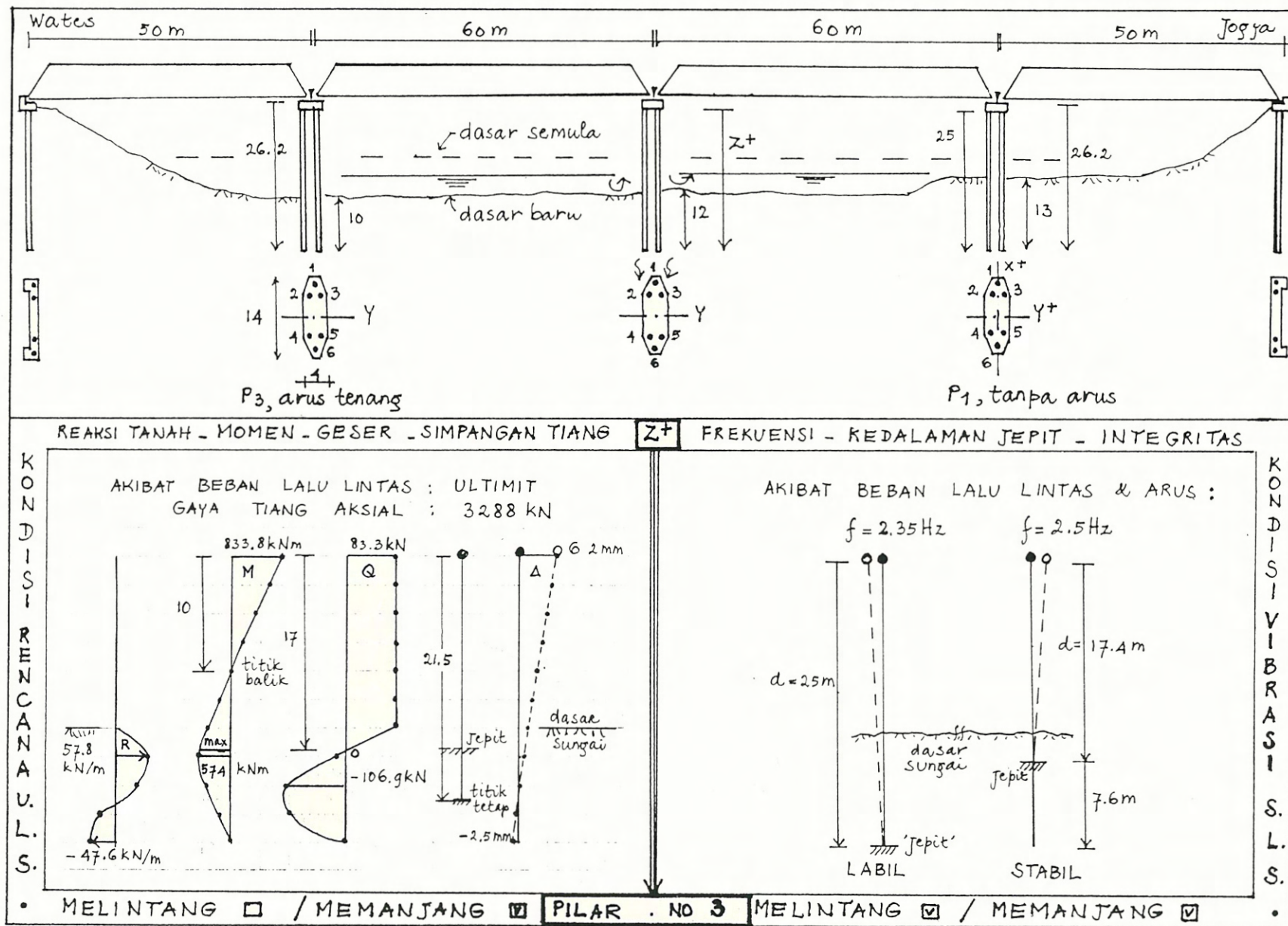


* hanya akibat arus sungai,
jembatan kosong

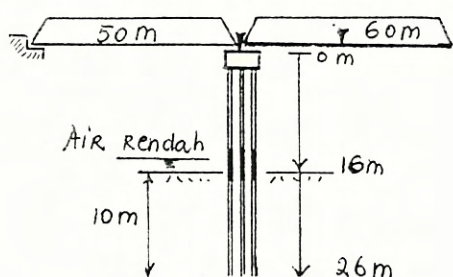
** jembatan bergetar arah vertikal



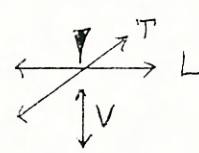
LAMPIRAN 4:
Pilar no.3 arah Jogja



TES GETAR PILAR DAN JEMBATAN (LALU LINTAS $\equiv$ * Rangkaian ☒ / satu ☐ TRUK)										
No.	Jembatan	Pondasi	Tinggi Pilar(m)		Arah	Frekwensi(Hertz)		Intensitas Getar		
			bebas	tertanam		Pilar	Jembatan	Pilar	Jembatan	Dimensi
4	Progo	Tiang bor	1	13m	L	2.5	5.26	0.020	0.02	Perpindah-an (mm) dinamik
					V	4.6	2	0.007	0.007	
					T	2.35	8.6	0.006	0.006	
					L		5		1.25	Kecepatan (mm/detik) getar
					V			1.3	2.5	
					T	2.7		0.4	1.5	

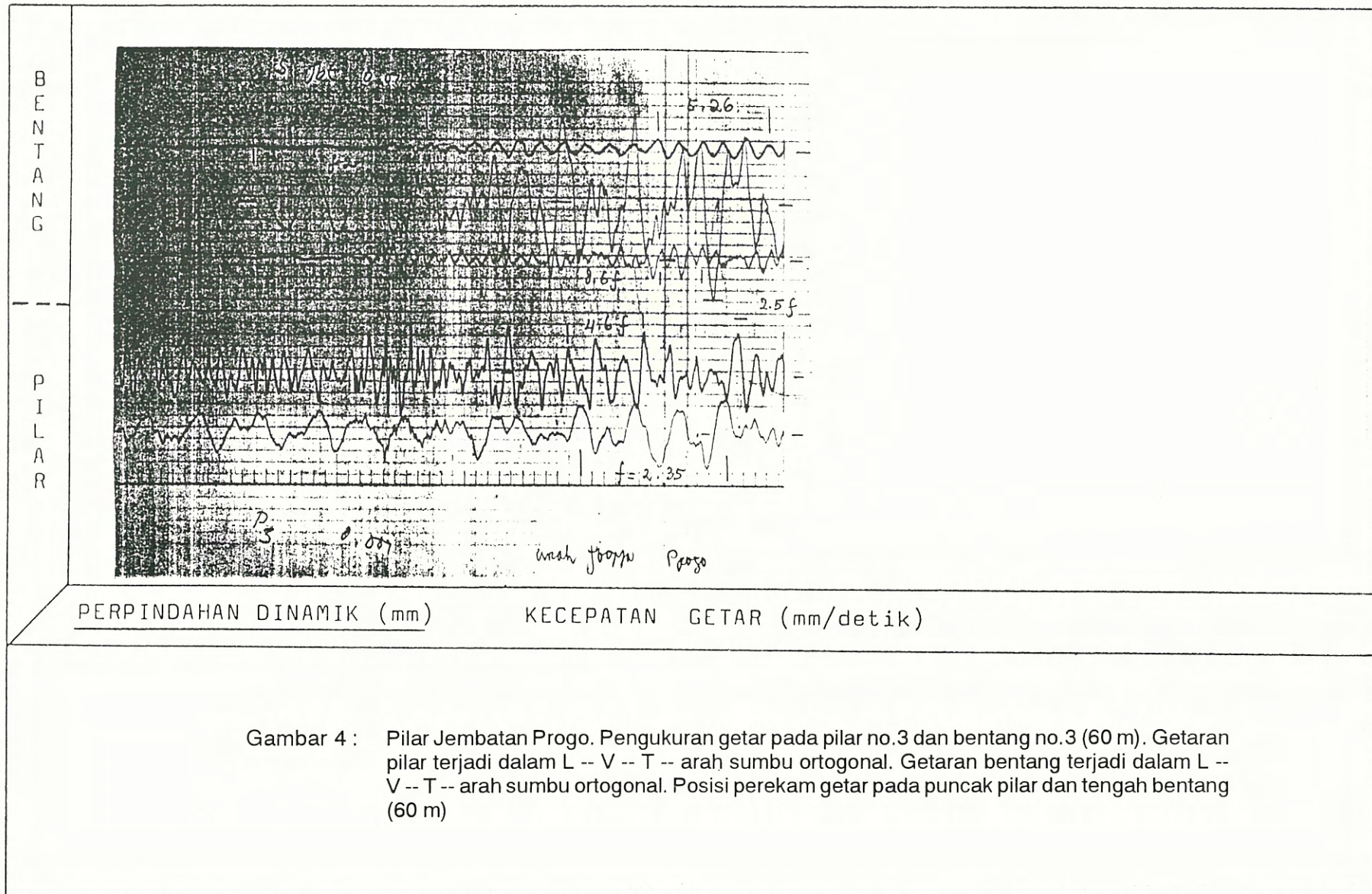
Wates  → Yogya

Pilar 3 arah Yogya



* Rangkaian lalu lintas





LAMPIRAN 5

Perhitungan tipikal dengan Program Komputer BMS

'PILAR JEMBATAN PROGO NO.2 ARAH WATES'
 'TIANG BOR 13M DIATAS DASAR SUNGAI KN.M'
 6 0 0 0
 'PROPERTIES'

1	0.04908	0.04908	0.0982	0.7853	1	1	29000000	0.25
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'RAKES'
 1 'VERTIKAL'
 'SOIL PROPERTIES'
 '****' 1 0
 0 0 'SAND' 0 0
 12.999 0
 13.0 0 'SAND' 15 10
 25.0 30000
 'PILES'

1	6.05	0	0	25	0	0	1	1	1	0	'FIX'	'REL'
2	3.55	-1.25	0	25	0	0	1	1	1	0	'FIX'	'REL'
3	3.55	-1.25	0	25	0	0	1	1	1	0	'FIX'	'REL'
4	-3.55	-1.25	0	25	0	0	1	1	1	2	'FIX'	'REL'
5	-3.55	-1.25	0	25	0	0	1	1	1	2	'FIX'	'REL'
6	-6.05	0	0	25	0	0	1	1	1	2	'FIX'	'REL'

'CONTINUE'
 'BEAN SENDIRI NOMINAL DAN ARUS MELINTANG ULTIMATE'

1	0	0	0	225	0	6948	0	2363	0
---	---	---	---	-----	---	------	---	------	---

'CONTINUE'
 'BEAN SENDIRI NOMINAL DAN ARUS MEMANJANG ULTIMATE'

1	0	0	0	0	225	6948	2363	0	0
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'END'

SNOWY MOUNTAINS ENGINEERING CORPORATION

Program PILING

Special Version

Analysis of Structural Piling System
 Bridge Management System - Design Manual

\bat\progo.plg

5:59 pm

6 Jan 93

PILAR JEMBATAN PROGO NO.2 ARAH WATES
 TIANG BOR 13M DIATAS DASAR SUNGAI KN.M

PILE PROPERTIES

No	IRR	ISS	J	A	BR	BS	E	PR
1	.491E-01	.491E-01	.982E-01	.785	1.000	1.000	.290E+08	.250

RAKES

RAKE NO. HORIZ. VERT.
1 *** VERTIKAL ***

SOIL PROPERTIES

Property No. 1 Soil Surface Z-Coord .000

Z. coord	Elastic Modulus	Soil Type	Cu (clay) Phi (sand)	Soil Density
.000	.000E+00	SAND	.000	.000
12.999	.000E+00	SAND	.000	.000
13.000	.000E+00	SAND	15.000	10.000
25.000	.300E+00	SAND	15.000	10.000

PILE DETAILS

NO.	X	Y	Z	LENG TH	AL PHA	GAM MA	RA KE	SEC	SOIL	TOP	BOT
1	6.050	.000	.000	25000	0	0	1	1	1	FIX	REL
2	3.550	-1250	.000	25000	0	0	1	1	1	FIX	REL
3	3.550	1250	.000	25000	0	0	1	1	1	FIX	REL
4	-3550	-1250	.000	25000	0	0	1	1	1	FIX	REL
5	-3550	1250	.000	25000	0	0	1	1	1	FIX	REL
6	-6050	.000	.000	25000	0	0	1	1	1	FIX	REL

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PILAR JEMBATAN PROGO NO.2 ARAH WATES
TIANG BOR 13M DIATAS DASAR SUNGAI KN M

Load Case 1

BEBAN SENDIRI NOMINAL DAN ARUS MELINTANG ULTIMATE

LOAD	X-ORD	Y-ORD	Z-ORD	FX	FY	FZ	MX	MY	MZ
1	000	000	000	225.0	0	6948.0	0	2363.0	0

GLOBAL DIPLACEMENT AT ORIGIN

X-DEF	Y-DEF	Z-DEF	X-ROT	Y-ROT	Z-ROT
.1711E-01	.0000E+00	.1271E-02	.0000E+00	.1392E-05	.0000E+00

PILE FORCES

PILE	R-SHEAR	S-SHEAR	AXIAL	R-MOMENT	S-MOMENT	TORSION
1	37.500	.000	1150.330	.000	367.715	.000
2	37.500	.000	1153.500	.000	367.715	.000
3	37.500	.000	1153.500	.000	367.715	.000
4	37.500	.000	1162.500	.000	367.715	.000
5	37.500	.000	1162.500	.000	367.715	.000
6	37.500	.000	1165.670	.000	367.715	.000

PILE HEAD DEFLECTIONS

PILE	X-ORD	Y-ORD	Z-ORD	X-DEF	Y-DEF	Z-DEF
1	6.050	.000	.000	.1711E-01	.0000E+00	.1263E-02
2	3.550	-1.250	.000	.1711E-01	.0000E+00	.1266E-02
3	3.550	1.250	.000	.1711E-01	.0000E+00	.1266E-02
4	-3.550	-1.250	.000	.1711E-01	.0000E+00	.1276E-02
5	-3.550	1.250	.000	.1711E-01	.0000E+00	.1276E-02
6	-6.050	.000	.000	.1711E-01	.0000E+00	.1280E-02

COORDINATE AND DEFLECTIONS OF LOAD POINTS

POINT	X-ORD	Y-ORD	Z-ORD	X-DEF	Y-DEF	Z-DEF
1	.000	.000	.000	.1711E-01	.0000E+00	.1271E-02

SNOWY MOUNTAINS ENGINEERING CORPORATION

Program PILING

Special Version

Analysis of Structural Piling Systems
 Bridge Management System - Design Manual

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PILAR JEMBATAN PROGO NO.2 ARAH WATES
 TIANG BOR 13M DIATAS DASAR SUNGAI KN.M

All Piles

Load Case 1

BEBAN SENDIRI NOMINAL DAN ARUS MELINTANG ULTIMATE

MAXIMUM SOIL PRESSURES s-t plane

Pile No	Surface Depth	Axiz Distance	Pressure	Ultimate	Cu(clay) Kp(sand)	Type	Soil No	Density
	25.00	25.00	.00	611.42	1.698	SAND	1	10.00
2	25.00	25.00	.00	611.42	1.698	SAND	1	10.00
3	25.00	25.00	.00	611.42	1.698	SAND	1	10.00
4	25.00	25.00	.00	611.42	1.698	SAND	1	10.00
5	25.00	25.00	.00	611.42	1.698	SAND	1	10.00
6	25.00	25.00	.00	611.42	1.698	SAND	1	10.00

MAXIMUM SOIL PRESSURES r-t plane

Pile No	Surface Depth	Axiz Distance	Pressure	Ultimate	Cu(clay) Kp(sand)	Type	Soil No	Density
1	25.00	25.00	-16.13	611.42	1.698	SAND	1	10.
2	25.00	25.00	-16.13	611.42	1.698	SAND	1	10.
3	25.00	25.00	-16.13	611.42	1.698	SAND	1	10.
4	25.00	25.00	-16.13	611.42	1.698	SAND	1	10.
5	25.00	25.00	-16.13	611.42	1.698	SAND	1	10.
6	25.00	25.00	-16.13	611.42	1.698	SAND	1	10.

Pile No. 4

Load Case 1

BEBAN SENDIRI NOMINAL DAN ARUS MELINTANG ULTIMATE

SOIL AND PILE REACTIONS s-t plane

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.00000	.00	.00	.00	SAND	.00	.00
1.25	.00000	.00	.00	.00	SAND	.00	.00
2.50	.00000	.00	.00	.00	SAND	.00	.00
3.75	.00000	.00	.00	.00	SAND	.00	.00
5.00	.00000	.00	.00	.00	SAND	.00	.00
6.25	.00000	.00	.00	.00	SAND	.00	.00
7.50	.00000	.00	.00	.00	SAND	.00	.00
8.75	.00000	.00	.00	.00	SAND	.00	.00
10.00	.00000	.00	.00	.00	SAND	.00	.00
11.25	.00000	.00	.00	.00	SAND	.00	.00
12.50	.00000	.00	.00	.00	SAND	.00	.00
13.75	.00000	.00	.00	38.21	SAND	.00	.00
15.00	.00000	.00	.00	101.90	SAND	.00	.00
16.25	.00000	.00	.00	165.59	SAND	.00	.00
17.50	.00000	.00	.00	229.28	SAND	.00	.00
18.75	.00000	.00	.00	292.97	SAND	.00	.00
20.00	.00000	.00	.00	356.66	SAND	.00	.00
21.25	.00000	.00	.00	420.35	SAND	.00	.00
22.50	.00000	.00	.00	484.04	SAND	.00	.00
23.75	.00000	.00	.00	547.73	SAND	.00	.00
25.00	.00000	.00#	.00	611.42	SAND	.00	.00

SOIL AND PILE REACTIONS r-t plane melintang

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.01692	.00	.00	.00	SAND	37.50	367.71
1.25	.01675	.00	.00	.00	SAND	37.50	320.84
2.50	.01623	.00	.00	.00	SAND	37.50	273.96
3.75	.01541	.00	.00	.00	SAND	37.50	227.09
5.00	.01434	.00	.00	.00	SAND	37.50	180.21
6.25	.01307	.00	.00	.00	SAND	37.50	133.34
7.50	.01166	.00	.00	.00	SAND	37.50	86.46
8.75	.01015	.00	.00	.00	SAND	37.50	39.59
10.00	.00860	.00	.00	.00	SAND	37.50	-7.29
11.25	.00705	.00	.00	.00	SAND	37.50	-54.16
12.50	.00557	.00	.00	.00	SAND	37.50	-101.04
13.75	.00419	8.08	6.46	38.21	SAND	29.42	-147.91
15.00	.00298	16.61	13.29	101.90	SAND	12.81	-184.69
16.25	.00197	18.54	14.83	165.59	SAND	-5.74	-200.69
17.50	.00117	15.66	12.53	229.28	SAND	-21.40	-193.52
18.75	.00058	10.11	8.09	292.97	SAND	-31.51	-166.77
20.00	.00017	3.65	2.92	356.66	SAND	-35.16	-127.38
21.25	-.00010	-2.62	-2.10	420.35	SAND	-32.54	-83.43
22.50	-.00028	-8.41	-6.73	484.04	SAND	-24.13	-42.76
23.75	-.00041	-14.05	-11.24	547.73	SAND	-10.08	-12.59
25.00	-.00052	-10.08#	-16.13	611.42	SAND	.00	.02

Pile No. 5

Load Case 1

BEBAN SENDIRI NOMINAL DAN ARUS MELINTANG ULTIMATE

SOIL AND PILE REACTIONS s-t plane

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.00000	.00	.00	.00	SAND	.00	.00
1.25	.00000	.00	.00	.00	SAND	.00	.00
2.50	.00000	.00	.00	.00	SAND	.00	.00
3.75	.00000	.00	.00	.00	SAND	.00	.00
5.00	.00000	.00	.00	.00	SAND	.00	.00
6.25	.00000	.00	.00	.00	SAND	.00	.00
7.50	.00000	.00	.00	.00	SAND	.00	.00
8.75	.00000	.00	.00	.00	SAND	.00	.00
10.00	.00000	.00	.00	.00	SAND	.00	.00
11.25	.00000	.00	.00	.00	SAND	.00	.00
12.50	.00000	.00	.00	.00	SAND	.00	.00
13.75	.00000	.00	.00	38.21	SAND	.00	.00
15.00	.00000	.00	.00	101.90	SAND	.00	.00
16.25	.00000	.00	.00	165.59	SAND	.00	.00
17.50	.00000	.00	.00	229.28	SAND	.00	.00
18.75	.00000	.00	.00	292.97	SAND	.00	.00
20.00	.00000	.00	.00	356.66	SAND	.00	.00
21.25	.00000	.00	.00	420.35	SAND	.00	.00
22.50	.00000	.00	.00	484.04	SAND	.00	.00
23.75	.00000	.00	.00	547.73	SAND	.00	.00
25.00	.00000	.00#	.00	611.42	SAND	.00	.00

SOIL AND PILE REACTIONS r-t plane

Axis	Lateral	----- SOIL -----				---- PILE ----	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.01692	.00	.00	.00	SAND	37.50	367.71
1.25	.01675	.00	.00	.00	SAND	37.50	320.84
2.50	.01623	.00	.00	.00	SAND	37.50	273.96
3.75	.01541	.00	.00	.00	SAND	37.50	227.09
5.00	.01434	.00	.00	.00	SAND	37.50	180.21
6.25	.01307	.00	.00	.00	SAND	37.50	133.34
7.50	.01166	.00	.00	.00	SAND	37.50	86.46
8.75	.01015	.00	.00	.00	SAND	37.50	39.59
10.00	.00860	.00	.00	.00	SAND	37.50	-7.29
11.25	.00705	.00	.00	.00	SAND	37.50	-54.16
12.50	.00557	.00	.00	.00	SAND	37.50	-101.04
13.75	.00419	8.08	6.46	38.21	SAND	29.42	-147.91
15.00	.00298	16.61	13.29	101.90	SAND	12.81	-184.69
16.25	.00197	18.54	14.83	165.59	SAND	-5.74	-200.69
17.50	.00117	15.66	12.53	229.28	SAND	-21.40	-193.52
18.75	.00058	10.11	8.09	292.97	SAND	-31.51	-166.77
20.00	.00017	3.65	2.92	356.66	SAND	-35.16	-127.38
21.25	-.00010	-2.62	-2.10	420.35	SAND	-32.54	-83.43
22.50	-.00028	-8.41	-6.73	484.04	SAND	-24.13	-42.76
23.75	-.00041	-14.05	-11.24	547.73	SAND	-10.08	-12.59
25.00	-.00052	-10.08#	-16.13	611.42	SAND	.00	.02

Pile No. 6

Load Case 1

BEBAN SENDIRI NOMINAL DAN ARUS MELINTANG ULTIMATE

SOIL AND PILE REACTIONS s-t plane

Axis	Lateral	----- SOIL -----				---- PILE ----	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.00000	.00	.00	.00	SAND	.00	.00
1.25	.00000	.00	.00	.00	SAND	.00	.00
2.50	.00000	.00	.00	.00	SAND	.00	.00
3.75	.00000	.00	.00	.00	SAND	.00	.00
5.00	.00000	.00	.00	.00	SAND	.00	.00
6.25	.00000	.00	.00	.00	SAND	.00	.00
7.50	.00000	.00	.00	.00	SAND	.00	.00
8.75	.00000	.00	.00	.00	SAND	.00	.00
10.00	.00000	.00	.00	.00	SAND	.00	.00
11.25	.00000	.00	.00	.00	SAND	.00	.00
12.50	.00000	.00	.00	.00	SAND	.00	.00
13.75	.00000	.00	.00	38.21	SAND	.00	.00
15.00	.00000	.00	.00	101.90	SAND	.00	.00
16.25	.00000	.00	.00	165.59	SAND	.00	.00
17.50	.00000	.00	.00	229.28	SAND	.00	.00
18.75	.00000	.00	.00	292.97	SAND	.00	.00
20.00	.00000	.00	.00	356.66	SAND	.00	.00
21.25	.00000	.00	.00	420.35	SAND	.00	.00
22.50	.00000	.00	.00	484.04	SAND	.00	.00
23.75	.00000	.00	.00	547.73	SAND	.00	.00
25.00	.00000	.00#	.00	611.42	SAND	.00	.00

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.01692	.00	.00	.00	SAND	37.50	367.71
1.25	.01675	.00	.00	.00	SAND	37.50	320.84
2.50	.01623	.00	.00	.00	SAND	37.50	273.96
3.75	.01541	.00	.00	.00	SAND	37.50	227.09
5.00	.01434	.00	.00	.00	SAND	37.50	180.21
6.25	.01307	.00	.00	.00	SAND	37.50	133.34
7.50	.01166	.00	.00	.00	SAND	37.50	86.46
8.75	.01015	.00	.00	.00	SAND	37.50	39.59
10.00	.00860	.00	.00	.00	SAND	37.50	-7.29
11.25	.00705	.00	.00	.00	SAND	37.50	-54.16
12.50	.00557	.00	.00	.00	SAND	37.50	-101.04
13.75	.00419	8.08	6.46	38.21	SAND	29.42	-147.91
15.00	.00298	16.61	13.29	101.90	SAND	12.81	-184.69
16.25	.00197	18.54	14.83	165.59	SAND	-5.74	-200.69
17.50	.00117	15.66	12.53	229.28	SAND	-21.40	-193.52
18.75	.00058	10.11	8.09	292.97	SAND	-31.51	-166.77
20.00	.00017	3.65	2.92	356.66	SAND	-35.16	-127.38
21.25	-.00010	-2.62	-2.10	420.35	SAND	-32.54	-83.43
22.50	-.00028	-8.41	-6.73	484.04	SAND	-24.13	-42.76
23.75	-.00041	-14.05	-11.24	547.73	SAND	-10.08	-12.59
25.00	-.00052	-10.08#	-16.13	611.42	SAND	.00	.02

SNOWY MOUNTAINS ENGINEERING CORPORATION

Program PILING

Special Version

Analysis of Structural Piling Systems
Bridge Management System - Design Manual

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6 Jan 93

PILAR JEMBATAN PROGO NO.2 ARAH WATES
TIANG BOR 13M DIATAS DASAR SUNGAI KN.M

Load Case 2
BEBAN SENDIRI NOMINAL DAN ARUS MEMANJANG ULTIMATE

LOAD	X-ORD	Y-ORD	Z-ORD	FX	FY	FZ	MX	MY	MZ
1	000	000	000	0	225.0	6948.0	2363.0	0	0

GLOBAL DIPLACEMENT AT ORIGIN

X-DEF	Y-DEF	Z-DEF	X-ROT	Y-ROT	Z-ROT
.0000E+00	.2443E-01	.1271E-02	.7460E-03	.0000E+00	.0000E+00

PILE FORCES

PILE	R-SHEAR	S-SHEAR	AXIAL	R-MOMENT	S-MOMENT	TORSION
1	.000	37.500	1158.000	-314.041	.000	.000
2	.000	37.500	308.551	-314.041	.000	.000
3	.000	37.500	2007.449	-314.041	.000	.000
4	.000	37.500	308.551	-314.041	.000	.000
5	.000	37.500	2007.449	-314.041	.000	.000
6	.000	37.500	1158.000	-314.041	.000	.000

PILE HEAD DEFLECTIONS

PILE	X-ORD	Y-ORD	Z-ORD	X-DEF	Y-DEF	Z-DEF
1	6.050	.000	.000	.0000E+00	2443E-01	.1271E-02
2	3.550	-1.250	.000	.0000E+00	2443E-01	.3387E-03
3	3.550	1.250	.000	.0000E+00	2443E-01	.2204E-02
4	-3.550	-1.250	.000	.0000E+00	2443E-01	.3387E-03
5	-3.550	1.250	.000	.0000E+00	2443E-01	.2204E-02
6	-6.050	.000	.000	.0000E+00	2443E-01	.1271E-02

CORDINATES AND DEFLECTIONS OF LOAD POINTS

POINT	X-ORD	Y-ORD	Z-ORD	X-DEF	Y-DEF	Z-DEF
1	.000	.000	.000	.0000E+00	.2443E-01	.1271E-02

SNOWY MOUNTAINS ENGINEERING CORPORATION

Program PILING

Special Version

Analysis of Structural Piling Systems
Bridge Management System - Design Manual

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6 Jan 93

PILAR JEMBATAN PROGO NO.2 ARAH WATES
TIANG BOR 13M DIATAS DASAR SUNGAI KN.M.

All Piles

Load Case 2

BEBAN SENDIRI NOMINAL DAN ARUS MEMANJANG ULTIMATE

MAXIMUM SOIL PRESSURES s-t plane

Pile No	Surface Depth	Axiz Distance	Pressure	Ultimate	Cu(clay) Kp(sand)	Type	Soil	Density
1	25.00	25.00	-18.26	611.42	1.698	SAND	1	10.00
2	25.00	25.00	-18.26	611.42	1.698	SAND	1	10.00
3	25.00	25.00	-18.26	611.42	1.698	SAND	1	10.00
4	25.00	25.00	-18.26	611.42	1.698	SAND	1	10.00
5	25.00	25.00	-18.26	611.42	1.698	SAND	1	10.00
6	25.00	25.00	-18.26	611.42	1.698	SAND	1	10.00

MAXIMUM SOIL PRESSURES r-t plane

Pile No	Surface Depth	Axiz Distance	Pressure	Ultimate	Cu(clay) Kp(sand)	Type	Soil	Density
1	25.00	25.00	.00	611.42	1.698	SAND	1	10.
2	25.00	25.00	.00	611.42	1.698	SAND	1	10.
3	25.00	25.00	.00	611.42	1.698	SAND	1	10.
4	25.00	25.00	.00	611.42	1.698	SAND	1	10.
5	25.00	25.00	.00	611.42	1.698	SAND	1	10.
6	25.00	25.00	.00	611.42	1.698	SAND	1	10.

Pile No. 4

Load Case 2

BEBAN SENDIRI NOMINAL DAN ARUS MEMANJANG ULTIMATE

SOIL AND PILE REACTIONS s-t plane

Axis	Lateral	----- SOIL -----				---- PILE ----	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.02406	.00	.00	.00	SAND	37.50	314.04
1.25	.02301	.00	.00	.00	SAND	37.50	267.17
2.50	.02166	.00	.00	.00	SAND	37.50	220.29
3.75	.02008	.00	.00	.00	SAND	37.50	173.42
5.00	.01830	.00	.00	.00	SAND	37.50	126.54
6.25	.01638	.00	.00	.00	SAND	37.50	79.67
7.50	.01438	.00	.00	.00	SAND	37.50	32.79
8.75	.01234	.00	.00	.00	SAND	37.50	-14.08
10.00	.01031	.00	.00	.00	SAND	37.50	-60.96
11.25	.00835	.00	.00	.00	SAND	37.50	-107.83
12.50	.00651	.00	.00	.00	SAND	37.50	-154.71
13.75	.00484	9.33	7.47	38.21	SAND	28.17	-201.58
15.00	.00339	18.93	15.14	101.90	SAND	9.24	-236.79
16.25	.00220	20.75	16.60	165.59	SAND	-11.51	-248.34
17.50	.00127	17.09	13.67	229.28	SAND	-28.60	-233.95
18.75	.00060	10.49	8.39	292.97	SAND	-39.09	-298.20
20.00	.00014	3.05	2.44	356.66	SAND	-42.14	-149.33
21.25	-.00015	-4.00	-3.20	420.35	SAND	-38.14	-96.66
22.50	-.00034	-10.34	-8.27	484.04	SAND	-27.79	-48.99
23.75	-.00048	-16.38	-13.10	547.73	SAND	-11.42	-14.25
25.00	-.00059	-11.42#	-18.26	611.42	SAND	.00	.02

SOIL AND PILE REACTIONS r-t plane

Axis	Lateral	----- SOIL -----				---- PILE ----	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.00000	.00	.00	.00	SAND	.00	.00
1.25	.00000	.00	.00	.00	SAND	.00	.00
2.50	.00000	.00	.00	.00	SAND	.00	.00
3.75	.00000	.00	.00	.00	SAND	.00	.00
5.00	.00000	.00	.00	.00	SAND	.00	.00
6.25	.00000	.00	.00	.00	SAND	.00	.00
7.50	.00000	.00	.00	.00	SAND	.00	.00
8.75	.00000	.00	.00	.00	SAND	.00	.00
10.00	.00000	.00	.00	.00	SAND	.00	.00
11.25	.00000	.00	.00	.00	SAND	.00	.00
12.50	.00000	.00	.00	.00	SAND	.00	.00
13.75	.00000	.00	.00	38.21	SAND	.00	.00
15.00	.00000	.00	.00	101.90	SAND	.00	.00
16.25	.00000	.00	.00	165.59	SAND	.00	.00
17.50	.00000	.00	.00	229.28	SAND	.00	.00
18.75	.00000	.00	.00	292.97	SAND	.00	.00
20.00	.00000	.00	.00	356.66	SAND	.00	.00
21.25	.00000	.00	.00	420.35	SAND	.00	.00
22.50	.00000	.00	.00	484.04	SAND	.00	.00
23.75	.00000	.00	.00	547.73	SAND	.00	.00
25.00	.00000	.00#	.00	611.42	SAND	.00	.00

File No. 5

Load Case 2

BEBAN SENDIRI NOMINAL DAN ARUS MEMANJANG ULTIMATE

SOIL AND PILE REACTIONS s-t plane

Axis	Lateral	----- SOIL -----				---- PILE ----	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.02406	.00	.00	.00	SAND	37.50	314.04
1.25	.02301	.00	.00	.00	SAND	37.50	267.17
2.50	.02166	.00	.00	.00	SAND	37.50	220.29
3.75	.02008	.00	.00	.00	SAND	37.50	173.42
5.00	.01830	.00	.00	.00	SAND	37.50	126.54
6.25	.01638	.00	.00	.00	SAND	37.50	79.67
7.50	.01438	.00	.00	.00	SAND	37.50	32.79
8.75	.01234	.00	.00	.00	SAND	37.50	-14.08
10.00	.01031	.00	.00	.00	SAND	37.50	-60.96
11.25	.00835	.00	.00	.00	SAND	37.50	-107.83
12.50	.00651	.00	.00	.00	SAND	37.50	-154.71
13.75	.00484	9.33	7.47	38.21	SAND	28.17	-201.58
15.00	.00339	18.93	15.14	101.90	SAND	9.24	-236.79
16.25	.00220	20.75	16.60	165.59	SAND	-11.51	-248.34
17.50	.00127	17.09	13.67	229.28	SAND	-28.60	-233.95
18.75	.00060	10.49	8.39	292.97	SAND	-39.09	-298.20
20.00	.00014	3.05	2.44	356.66	SAND	-42.14	-149.33
21.25	-.00015	-4.00	-3.20	420.35	SAND	-38.14	-96.66
22.50	-.00034	-10.34	-8.27	484.04	SAND	-27.79	-48.99
23.75	-.00048	-16.38	-13.10	547.73	SAND	-11.42	-14.25
25.00	-.00059	-11.42#	-18.26	611.42	SAND	.00	.02

SOIL AND PILE REACTIONS r-t plane

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.00000	.00	.00	.00	SAND	.00	.00
1.25	.00000	.00	.00	.00	SAND	.00	.00
2.50	.00000	.00	.00	.00	SAND	.00	.00
3.75	.00000	.00	.00	.00	SAND	.00	.00
5.00	.00000	.00	.00	.00	SAND	.00	.00
6.25	.00000	.00	.00	.00	SAND	.00	.00
7.50	.00000	.00	.00	.00	SAND	.00	.00
8.75	.00000	.00	.00	.00	SAND	.00	.00
10.00	.00000	.00	.00	.00	SAND	.00	.00
11.25	.00000	.00	.00	.00	SAND	.00	.00
12.50	.00000	.00	.00	.00	SAND	.00	.00
13.75	.00000	.00	.00	38.21	SAND	.00	.00
15.00	.00000	.00	.00	101.90	SAND	.00	.00
16.25	.00000	.00	.00	165.59	SAND	.00	.00
17.50	.00000	.00	.00	229.28	SAND	.00	.00
18.75	.00000	.00	.00	292.97	SAND	.00	.00
20.00	.00000	.00	.00	356.66	SAND	.00	.00
21.25	.00000	.00	.00	420.35	SAND	.00	.00
22.50	.00000	.00	.00	484.04	SAND	.00	.00
23.75	.00000	.00	.00	547.73	SAND	.00	.00
25.00	.00000	.00#	.00	611.42	SAND	.00	.00

Pile No. 6

Load Case 2

BEBAN SENDIRI NOMINAL DAN ARUS MEMANJANG ULTIMATE

SOIL AND PILE REACTIONS s-t plane

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.02406	.00	.00	.00	SAND	37.50	314.04
1.25	.02301	.00	.00	.00	SAND	37.50	267.17
2.50	.02166	.00	.00	.00	SAND	37.50	220.29
3.75	.02008	.00	.00	.00	SAND	37.50	173.42
5.00	.01830	.00	.00	.00	SAND	37.50	126.54
6.25	.01638	.00	.00	.00	SAND	37.50	79.67
7.50	.01438	.00	.00	.00	SAND	37.50	32.79
8.75	.01234	.00	.00	.00	SAND	37.50	-14.08
10.00	.01031	.00	.00	.00	SAND	37.50	-60.96
11.25	.00835	.00	.00	.00	SAND	37.50	-107.83
12.50	.00651	.00	.00	.00	SAND	37.50	-154.71
13.75	.00484	9.33	7.47	38.21	SAND	28.17	-201.58
15.00	.00339	18.93	15.14	101.90	SAND	9.24	-236.79
16.25	.00220	20.75	16.60	165.59	SAND	-11.51	-248.34
17.50	.00127	17.09	13.67	229.28	SAND	-28.60	-233.95
18.75	.00060	10.49	8.39	292.97	SAND	-39.09	-298.20
20.00	.00014	3.05	2.44	356.66	SAND	-42.14	-149.33
21.25	-.00015	-4.00	-3.20	420.35	SAND	-38.14	-96.66
22.50	-.00034	-10.34	-8.27	484.04	SAND	-27.79	-48.99
23.75	-.00048	-16.38	-13.10	547.73	SAND	-11.42	-14.25
25.00	-.00059	-11.42#	-18.26	611.42	SAND	.00	.02

SOIL AND PILE REACTIONS r-t plane

Axis	Lateral	----- SOIL -----				--- PILE ---	
Distance	Displ	Reaction	Pressure	Ultimate	Type	Shear	Moment
.00	.00000	.00	.00	.00	SAND	.00	.00
1.25	.00000	.00	.00	.00	SAND	.00	.00
2.50	.00000	.00	.00	.00	SAND	.00	.00
3.75	.00000	.00	.00	.00	SAND	.00	.00
5.00	.00000	.00	.00	.00	SAND	.00	.00
6.25	.00000	.00	.00	.00	SAND	.00	.00
7.50	.00000	.00	.00	.00	SAND	.00	.00
8.75	.00000	.00	.00	.00	SAND	.00	.00
10.00	.00000	.00	.00	.00	SAND	.00	.00
11.25	.00000	.00	.00	.00	SAND	.00	.00
12.50	.00000	.00	.00	.00	SAND	.00	.00
13.75	.00000	.00	.00	38.21	SAND	.00	.00
15.00	.00000	.00	.00	101.90	SAND	.00	.00
16.25	.00000	.00	.00	165.59	SAND	.00	.00
17.50	.00000	.00	.00	229.28	SAND	.00	.00
18.75	.00000	.00	.00	292.97	SAND	.00	.00
20.00	.00000	.00	.00	356.66	SAND	.00	.00
21.25	.00000	.00	.00	420.35	SAND	.00	.00
22.50	.00000	.00	.00	484.04	SAND	.00	.00
23.75	.00000	.00	.00	547.73	SAND	.00	.00
25.00	.00000	.00#	.00	611.42	SAND	.00	.00

Total Run time 1m. 04.1s